

CONDIZIONE NECESSARIA PER L'EQUILIBRIO MA NON SUFFICIENTE:

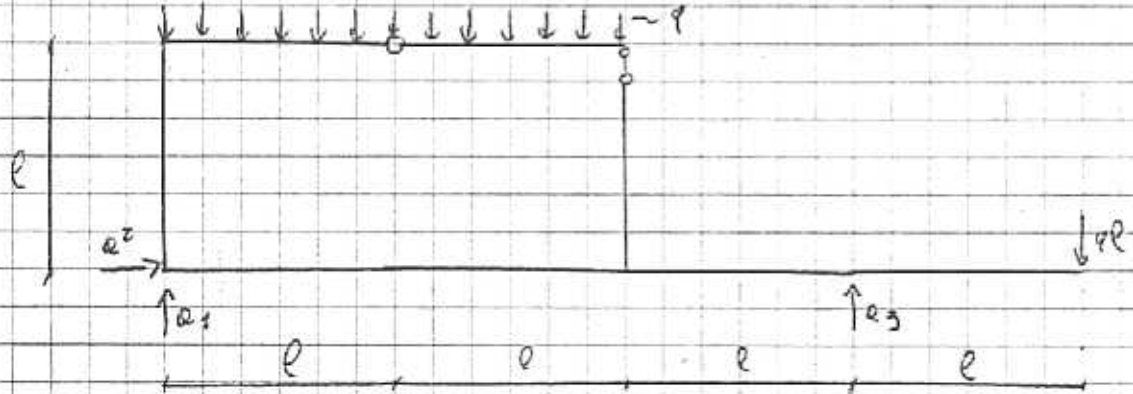
$$D + 3(m-1) \geq 3 + n_s$$

$$D = 3$$

$$m = 2 \quad 3 + 3(2-1) \geq 3 + 3$$

$n_s = 3 \quad 6 = 6$ la condizione necessaria è verificata ✓

Si sostituiscono ai vincoli le reazioni vincolari incognite e si risolve senza aprire la trave.



$$\begin{cases} a_2 = 0 \\ a_1 + a_3 - q \cdot 2l - ql = 0 \end{cases}
 \quad
 \begin{cases} a_2 = 0 \\ a_1 = ql \\ a_3 = \frac{2 \cdot 6 \cdot ql}{3} = 2ql \end{cases}$$

A) $-q \cdot 2l \cdot l - ql \cdot l + a_3 \cdot 3l = 0$ ✓

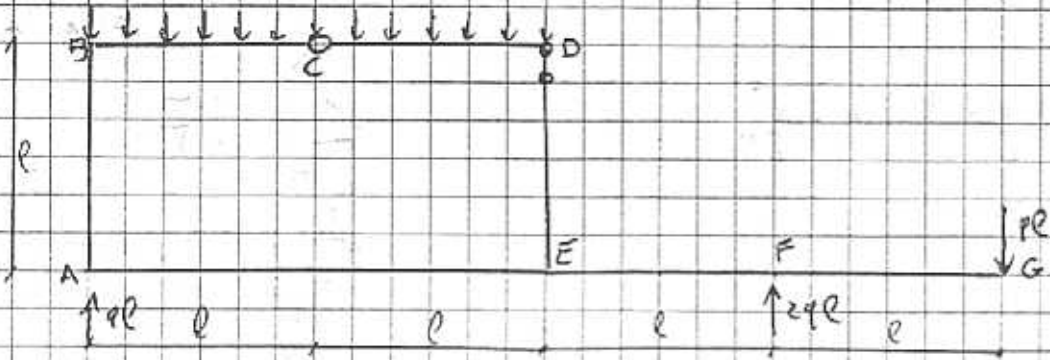
⇒ Come già affermato il testo, la trave è ISOSTATICA ESTERNAMENTE SE NON CI SONO LABILITÀ NELLA PORTIONE CHIUSA //

VERIFICA DIMENSIONALE:

$$a_1 = ql \rightarrow \frac{[F]}{[L]} \cdot [L] \text{ OK}$$

$$a_3 = 2ql \quad \frac{[F]}{[L]} \cdot [L] = [F] \text{ OK}$$

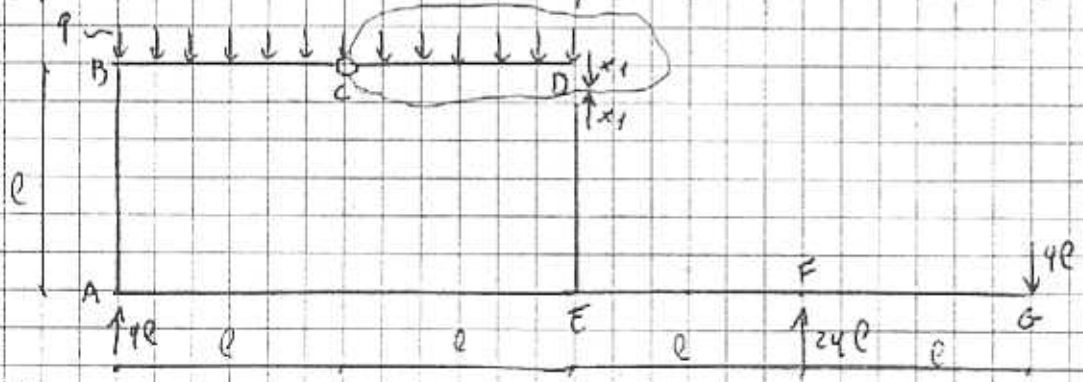
ASSETTO STATICO PER LA TRAVATURA CHIUSA:



VERIFICA ASSETTO STATICO:

$$\begin{cases} \sum \mathcal{O} = 0 \\ qL - qL + 24qL - 24qL = 0 \quad \text{OK} \\ G) (-qL \cdot 4L - 24qL + 24qL \cdot 3L = -64qL^2 + 64qL^2 = 0 \quad \text{OK} \end{cases}$$

Opro la travatura in prossimità della licella in D



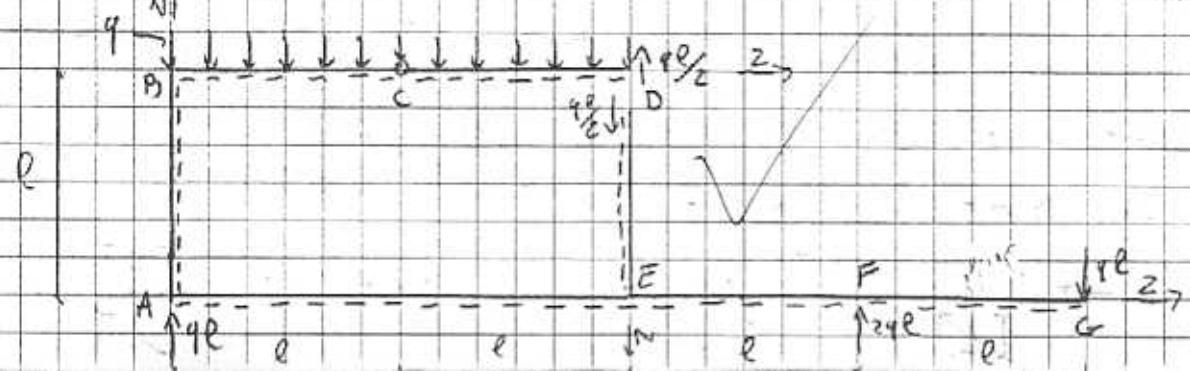
Ho già usato 2 equazioni ausiliarie me ne rimane ancora 1 calcolo il momento in c

$$M_c = 0 \quad \left\{ -x_1 \cdot \frac{L}{2} - qL \cdot \frac{L}{2} = 0 \quad x_1 = -\frac{4qL}{2} \right.$$

VERIFICA: (prendo l'altra parte di travatura)

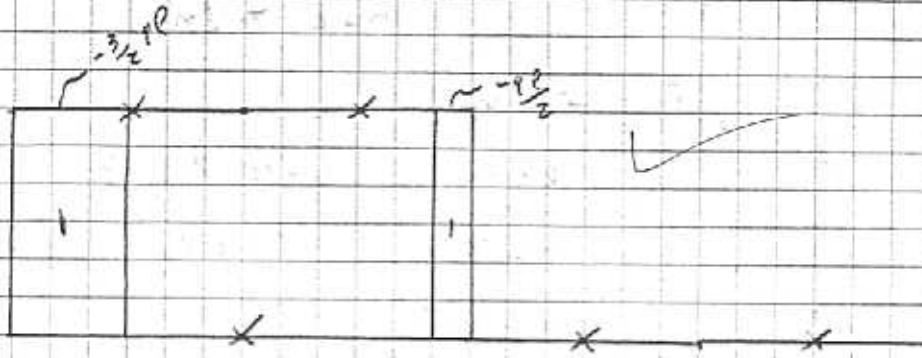
$$M_c = 0 \quad \frac{qL \cdot L}{2} - qL + 24qL \cdot 2L - qL \cdot 3L - \frac{qL \cdot L}{2} = 0 \quad \text{OK}$$

ASSETTO STATICO PER LA TRAVATURA APERTA:

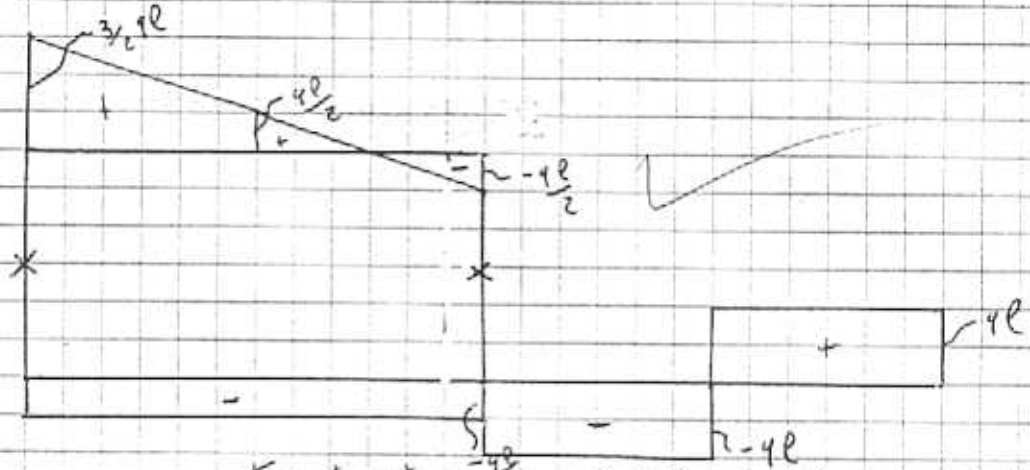


DIAGRAMMI DELLE CARATTERISTICHE DI SOLLECITAZIONE:

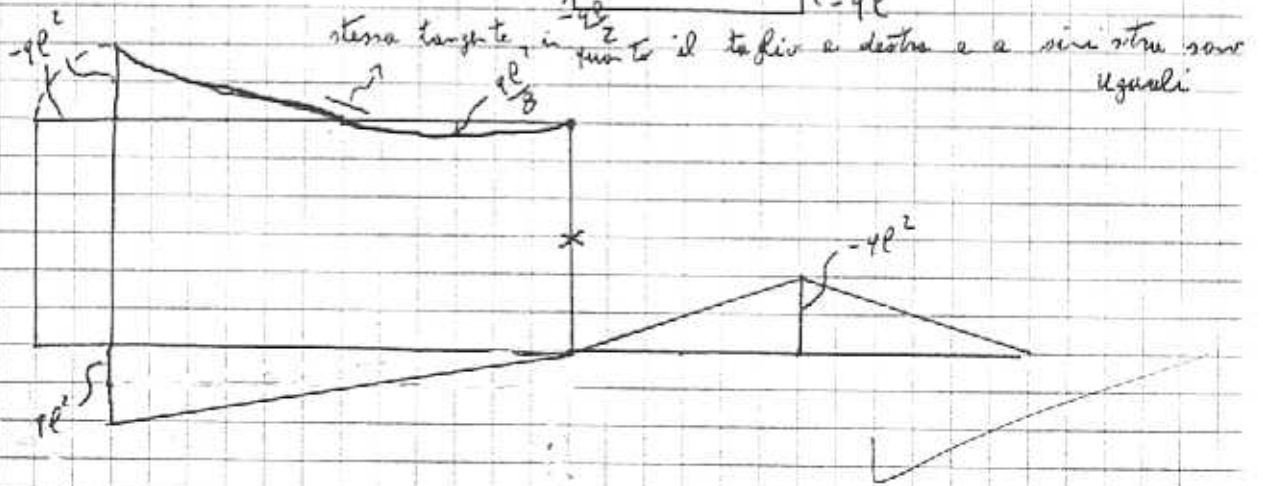
$N(z)$



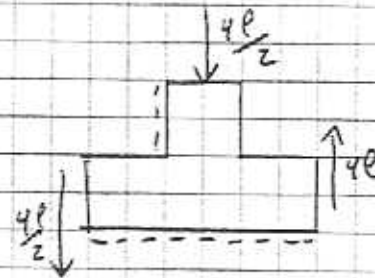
$T(z)$



$M(z)$

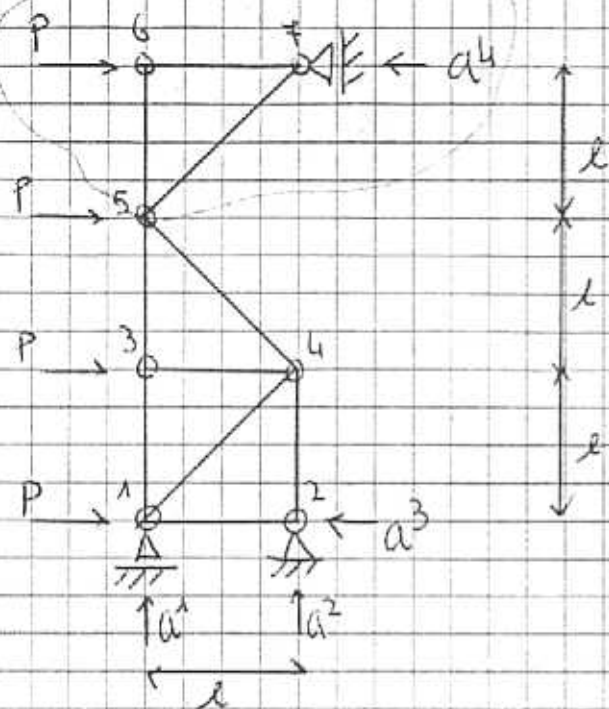


VERIFICA AL NODO E:



$$ql - \frac{ql}{2} - \frac{ql}{2} = 0 \quad \text{OK}$$

Problema 2)



1)

- $\lambda = 4$ (numero vincoli semplici)
- $n = 7$ (numero nodi)
- $a = 10$ (numero aste)

$$\lambda + a \geq 2n$$

$$4 + 10 \geq 2 \cdot 7 \rightarrow 14 = 14$$

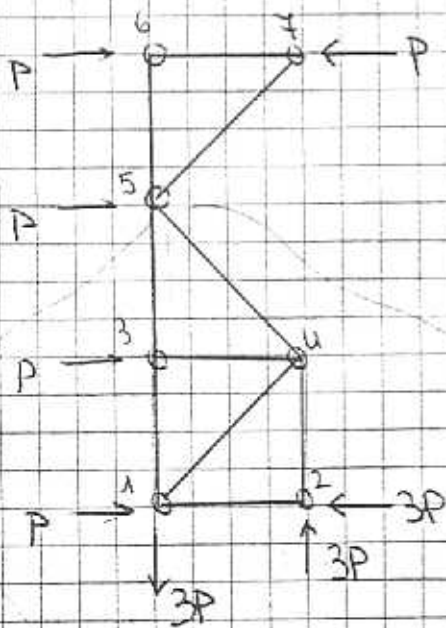
Condizione necessaria a per l'equilibrio è soddisfatta

- Determiniamo le reazioni vincolari tramite le tre equazioni cardinali della Statica più l'equazione algebrica relativa alla cerniera in 5

$$(1) \begin{cases} a^1 + a^2 = 0 \\ a^3 + a^4 - P - P - P - P = 0 \\ + a^2 \cdot \cancel{\ell} - P \cdot \cancel{\ell} - P \cdot 2\cancel{\ell} - P \cdot 3\cancel{\ell} + a^4 \cdot 3\cancel{\ell} = 0 \\ M_5 = 0 \quad + a^4 \cdot \cancel{\ell} - P \cdot \cancel{\ell} = 0 \end{cases}$$

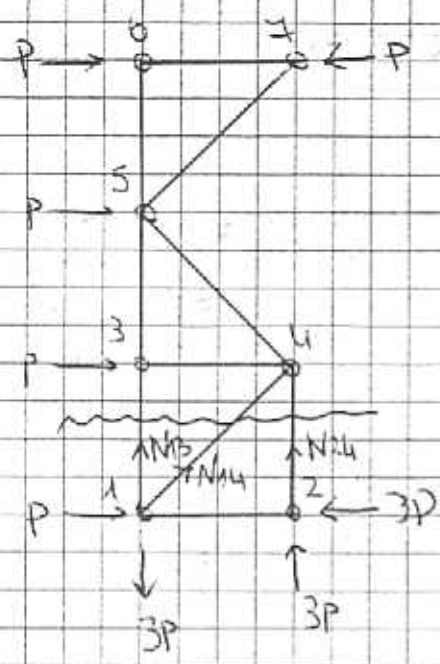
$$\begin{cases} a^1 = -a^2 = -3P \\ a^3 = 4P - a^4 = 3P \\ a^2 = 6P - 3a^4 = 3P \\ a^4 = P \end{cases}$$

- Assetto statico e vincolate



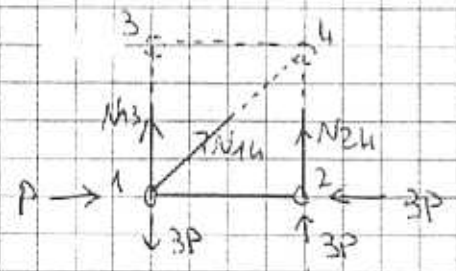
$$(2) \begin{cases} 3P - 3P = 0 \\ 4P - P - 3P = 0 \\ M_5 = 0 \quad P \cdot 3\ell + 3P \cdot \ell - P \cdot \ell - P \cdot 2\ell - P \cdot 3\ell = 0 \\ P \cdot \ell + P \cdot 2\ell + 3P \cdot \ell - 3P \cdot 2\ell = 0 \end{cases}$$

2)



asta	N
N24	-3P
N13	P
N14	$2\sqrt{2}P$
N35	P
N34	-P
N67	-P
N75	0
N65	0
N54	$-\sqrt{2}P$
N12	-3P

Sezione di Ritter sulle aste 13, 14, 24



Impongo le tre equazioni sui momenti nei nodi:

$$\begin{cases}
 (1) & 3P \cdot l + N_{24} \cdot l = 0 \\
 (4) & -N_{13} \cdot l + P \cdot l + 3P \cdot l - 3P \cdot l = 0 \\
 (1) & P - 3P + N_{14} \frac{\sqrt{2}}{2} = 0
 \end{cases}
 \rightarrow
 \begin{cases}
 N_{24} = -3P \\
 N_{13} = P \\
 N_{14} = 2\sqrt{2}P
 \end{cases}$$

↳ equivalente alla traslazione orizzontale

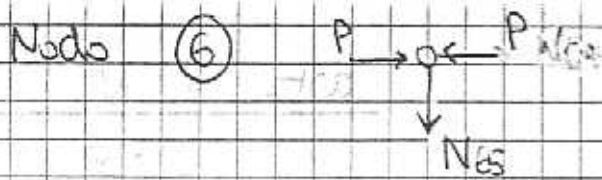
Continua la risoluzione della travatura utilizzando il metodo dei nodi conici.

Nodo (3)

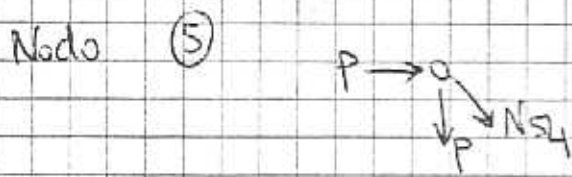
$$\begin{cases}
 N_{35} = P \\
 N_{34} = -P
 \end{cases}$$

Nodo (7)

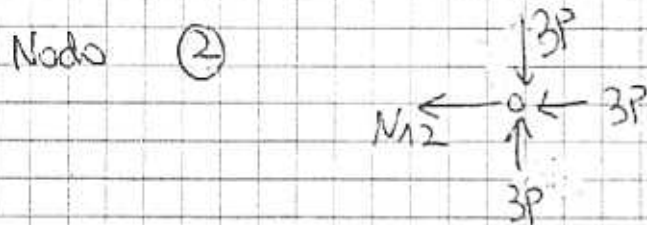
$$\begin{cases}
 P + N_{67} + \frac{\sqrt{2}}{2} N_{75} = 0 \\
 \frac{\sqrt{2}}{2} N_{75} = 0
 \end{cases}
 \rightarrow
 \begin{cases}
 N_{67} = -P \\
 N_{75} = 0
 \end{cases}$$



$$\left. \begin{aligned} P/P &= 0 \text{ ok} \\ N_{65} &= 0 \end{aligned} \right\} \rightarrow \text{ok}$$

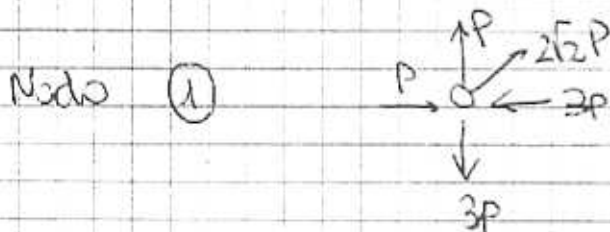


$$\left. \begin{aligned} P + \frac{\sqrt{2}}{2} N_{54} &= 0 \\ P + \frac{\sqrt{2}}{2} N_{54} &= 0 \end{aligned} \right\} \rightarrow N_{54} = -\sqrt{2}P$$

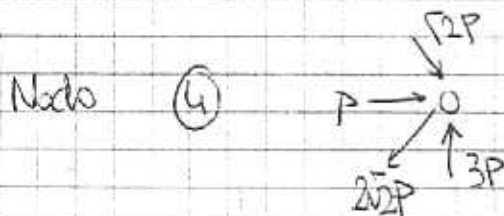


$$\left. \begin{aligned} 3P &= 3P \text{ ok} \\ 3P + N_{12} &= 0 \end{aligned} \right\} \rightarrow N_{12} = -3P$$

Studio, come verifica, il nodo ① e il nodo ④



$$\left. \begin{aligned} P - 3P + 2\sqrt{2} \cdot \frac{\sqrt{2}}{2} P &= 0 \\ P - 3P + 2\sqrt{2} \cdot \frac{\sqrt{2}}{2} P &= 0 \end{aligned} \right\} \text{ok}$$

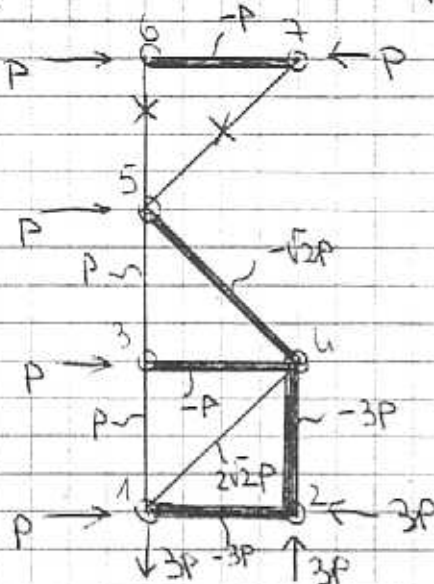


$$\left. \begin{aligned} P + \sqrt{2}P \cdot \frac{\sqrt{2}}{2} - 2\sqrt{2}P \cdot \frac{\sqrt{2}}{2} &= 0 \\ 3P - 2\sqrt{2}P \cdot \frac{\sqrt{2}}{2} - \sqrt{2}P \cdot \frac{\sqrt{2}}{2} &= 0 \end{aligned} \right\} \text{ok}$$

3) Diagrammi delle caratteristiche di sollecitazione (N)

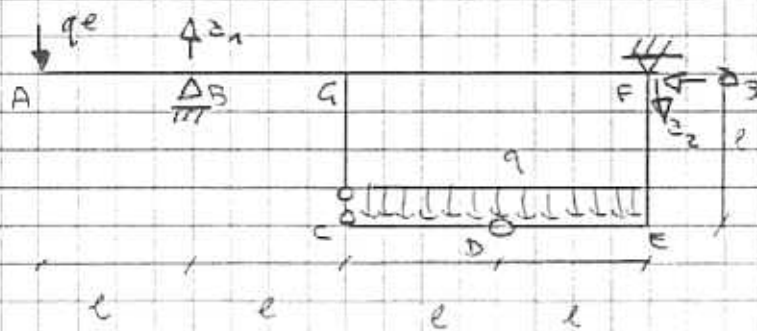
N positivo \rightarrow tratto sottile \rightarrow TIRANTI

N negativo \rightarrow tratto spesso \rightarrow PUNTONI



Problema 1

Travatura chiusa



$$\Delta + 3(m-1) \geq 3 + m_s$$

$$\Delta = 3$$

$$m = 2$$

$$m_s = 3 \quad (1+2)$$

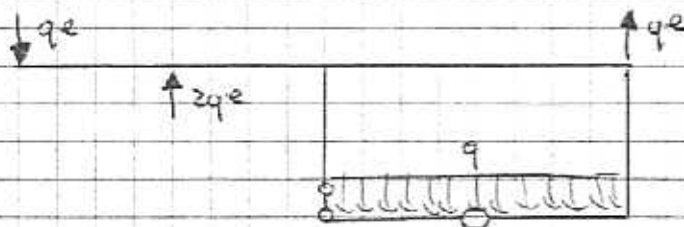
$\rightarrow 6 = 6$ condiz. necess. per l'equilibrio (isostatico)
 ✓ soddisfatta

Riesco a determinare le rest. vincolari ($\Delta = 3$)

$$\begin{cases} a_1 - qe - 2qe - a_2 = 0 \\ -a_3 = 0 \end{cases} \Rightarrow \begin{cases} a_2 = -qe \quad \checkmark \\ a_3 = 0 \quad \checkmark \end{cases}$$

$$(F) \quad 2qe \cdot e - a_1 \cdot 3e + qe \cdot 4e = 0 \Rightarrow a_1 = \frac{6qe}{3} = 2qe \quad \checkmark$$

Asse statico esterno



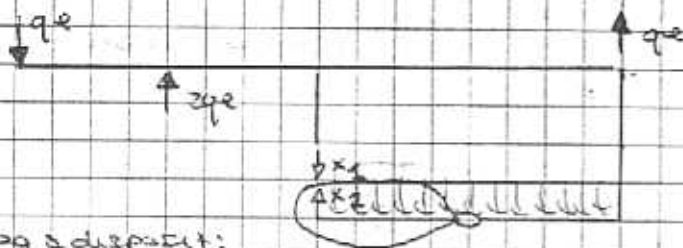
Verifiche DIM $2qe = \frac{F \cdot k}{k} \quad \checkmark \quad \checkmark$

$$qe = \frac{F \cdot k}{k} \quad \checkmark$$

$$\checkmark \begin{cases} -qe + 2qe + qe - 2qe = 0 \quad \checkmark \\ 0 = 0 \quad \checkmark \end{cases} \quad \text{ok}$$

$$(A) \quad 2qe \cdot e - 2qe \cdot 3e + qe \cdot 4e = 0 \quad \checkmark$$

Apno R_3 travatura int c (scansione) con $(m-1)$ tagli



velone ag a destra:

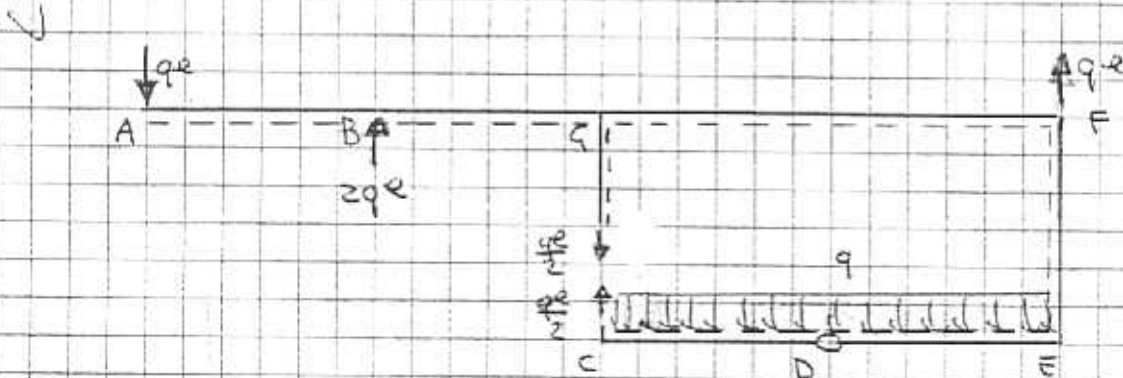
$$M_D = 0 \quad -x_1 q_e + \frac{q_e x_1^2}{2} = 0 \rightarrow x_1 = \frac{q_e}{2} \checkmark$$

✓ Verifica dell'altra parte della travatura:

$$M_D = 0 \quad -\frac{q_e x_1^2}{2} + q_e x_1 - 2q_e x_1 + q_e (3l - x_1) + x_1 q_e = 0$$

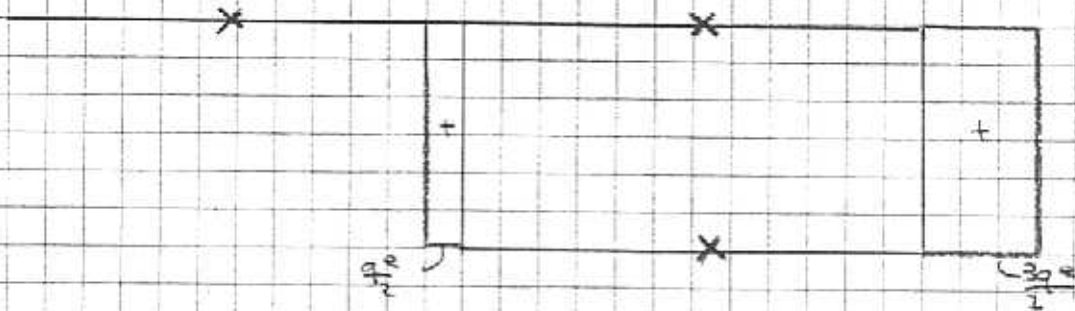
$$x_1 = -\frac{3q_e}{2} + \frac{q_e}{2} = -q_e \checkmark \quad \frac{F}{K} \checkmark \checkmark$$

Ascello statico female



Diagrammi

(N) Normale ✓



Tutto il tratto AC

non è soggetto a forze normali (disaccoppiamento solo a taglio in B)

Il tratto cE ha $N = \text{cost} (q_2(R) = 0) = \frac{q_e}{2} \rightarrow$ PERCHÉ? ✓

⊗ EQUIL? ⊗

VA SPIEGATO

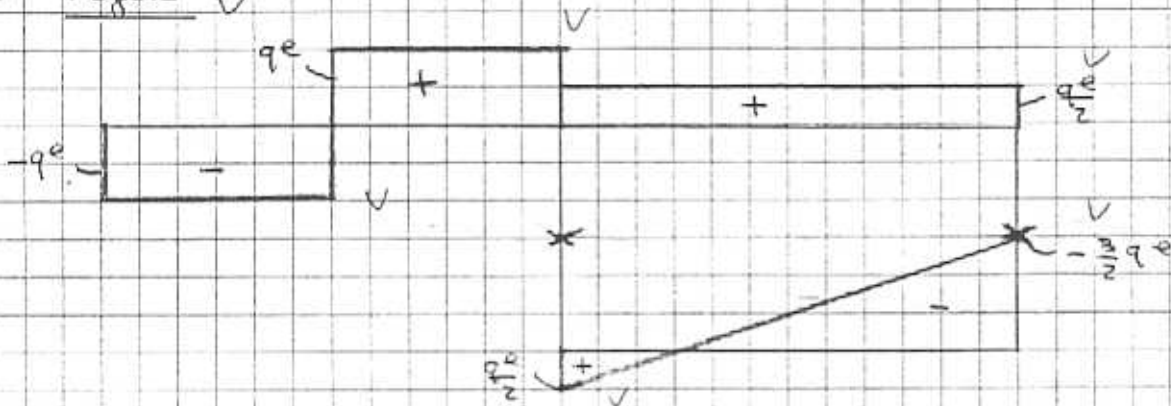
Il tratto \overline{GF} non è nuovamente soggetto a forza Normale

Il tratto \overline{EF} ha forza $N = \text{costante}$

$$N = qe - \frac{qe}{2} + 2qe - qe = \frac{3}{2}qe$$

I tratti CD e ED non sono soggetti a forza normale

Ⓘ Taglio V



\overline{AB} $q_y(x) = 0 \rightarrow T \text{ cost}$ $T = -qe$ \rightarrow PERCHÉ? VA SPIEGATO

\overline{BC} $q_y(x) = 0 \rightarrow T \text{ cost}$ $T = -qe + 2qe = qe$

\overline{CG} $T = 0$ (per la scomposizione)

\overline{GF} $q_y(x) = 0 \rightarrow T \text{ cost}$ $T = -qe + 2qe - \frac{qe}{2} = \frac{qe}{2}$

\overline{FE} $q_y(x) = 0 \rightarrow$ Il tratto \overline{FE} NON è soggetto a Taglio

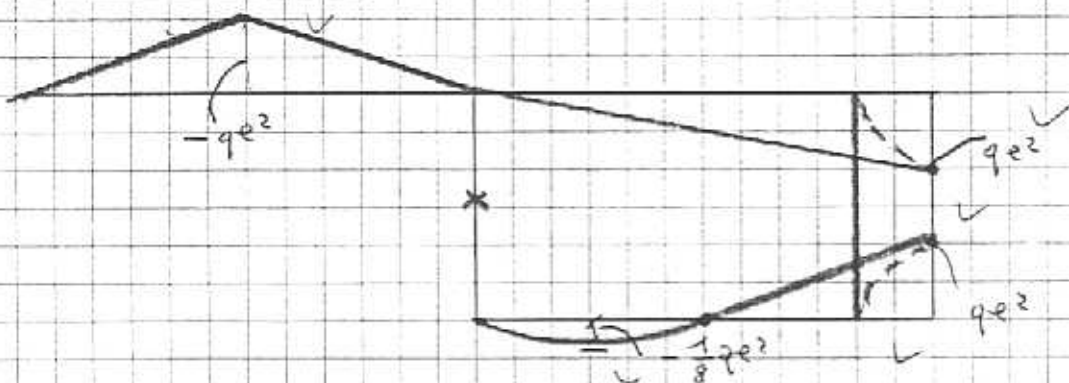
\overline{CE} (è armatura non rappresenta una discontinuità a Taglio)

$q_y(x) = \text{cost}$; $T = \text{lineare}$

$$T(E) = -qe + \frac{qe}{2} - 2qe + qe = -\frac{3}{2}qe$$

$$T(C) = \frac{qe}{2}$$

Ⓜ Momento flettente ✓



\overline{AB} $T \text{ costante} \rightarrow M \text{ lineare}$ $M(A) = 0$ $M(B) = -qe^2$

\overline{BQ} T cost \rightarrow H. element $T(B) = -qe^2$ $M(G) = -qeze + 2qe^2 = 0$

\overline{CQ} T=0 \rightarrow H. cost $M=0$

\overline{QF} T=cost \rightarrow H. element $M(G) = 0$

$$M(F) = -qeze + 2qeze - \frac{qeze}{x} = qe^2$$

\overline{FE} T=0 \rightarrow H. cost $M(F) = qe^2$

\overline{EC} T = element \rightarrow M = quadratic

$$M(a) = -qe^z - \frac{qe}{2}(2e-z) + 2qe(3e-z) - qe(4e-z) + \frac{qz^2}{2}$$

$$= \underbrace{-qe^z - qe^2 + \frac{qe^z}{2}} + \underbrace{6qe^2 - 2qe^z - 4qe^2 + qe^z} + \underbrace{\frac{qz^2}{2}}$$

$$M(z) = \frac{qz^2}{2} - \frac{3}{2}qe^z + qe^2 \quad \checkmark$$

$$M'(z) = qe^2$$

$$M(0) = 0 \quad \text{CERNIERA} \quad \checkmark \quad \checkmark$$

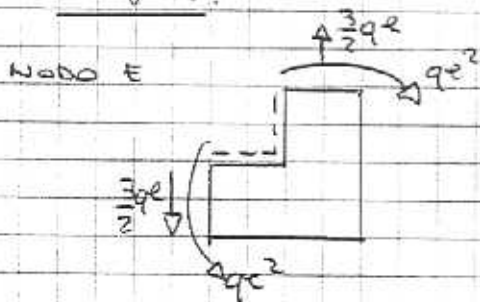
$$M(e) = 0 \quad \checkmark$$

$$M'(z) = qz - \frac{3}{2}qe = 0 \rightarrow z = \frac{3}{2}e \quad \checkmark \quad \begin{matrix} \text{MIN} \\ \text{MAX} \\ \text{FLESSO} \end{matrix}$$

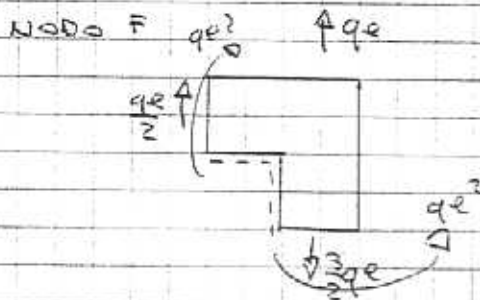
$$M''(z) = q > 0 \Rightarrow \text{MIN} \quad \checkmark$$

$$M(z = \frac{3}{2}e) = \frac{q}{2} \frac{9}{4} e^2 - \frac{3}{2} qe \frac{3}{2} e + qe^2 = qe^2 \left(\frac{9}{8} - \frac{9}{4} + 1 \right) = -\frac{1}{8} qe^2 \quad \checkmark$$

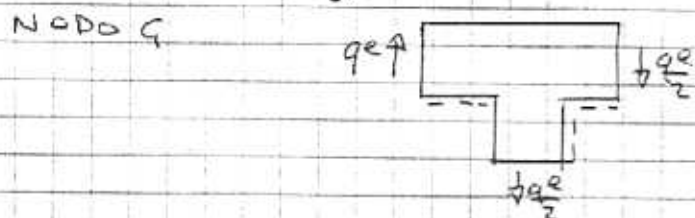
Var. f. c.



$$\begin{cases} \frac{3}{2} qe - \frac{3}{2} qe = 0 \quad \checkmark \\ 0 = 0 \quad \checkmark \\ qe^2 - qe^2 = 0 \quad \checkmark \end{cases} \quad \text{OK}$$

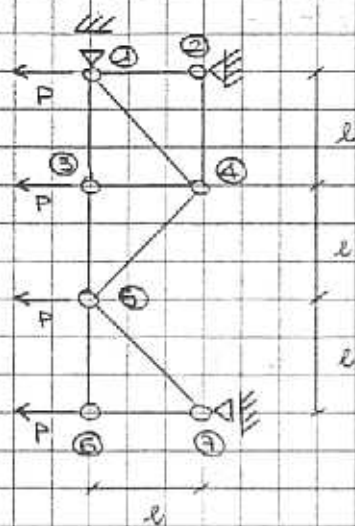


$$\begin{cases} qe + \frac{qe}{2} - \frac{3}{2} qe = 0 \quad \checkmark \\ qe^2 - qe^2 = 0 \quad \checkmark \\ 0 = 0 \quad \checkmark \end{cases} \quad \text{OK}$$



$$\begin{cases} 0 = 0 \quad \checkmark \\ qe - \frac{qe}{2} - \frac{qe}{2} = 0 \quad \checkmark \\ 0 = 0 \quad \checkmark \end{cases} \quad \text{OK}$$

Problema 2



$$a = m^{\circ} \text{ aste} = 10$$

$$m = m^{\circ} \text{ modi} = 7$$

$$s = m^{\circ} \text{ vincoli esterni} = 4$$

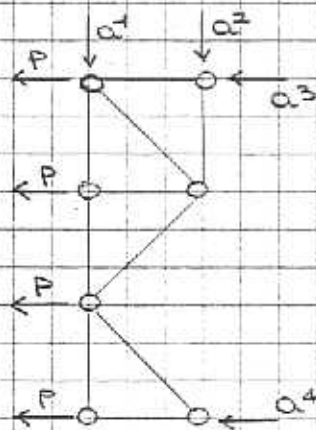
✓ • la struttura è una trave trussata, perciò verificiamo
 nec. ma non suff.

la condizione di esistenza dell'equilibrio: $s + a \geq 2m$

$$4 + 10 \geq 2 \cdot 7 \Rightarrow 7 = 7$$

la condizione necessaria ma non sufficiente per
 l'esistenza dell'equilibrio ISOSTATICO è soddisfatta.

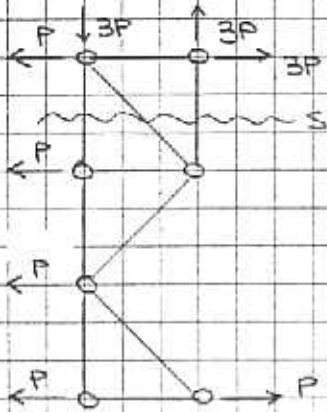
Le incognite determinate dalle azioni esercitate dai
 vincoli sono 4. Posso provare a trovarle ugualmente
 notando che in S ho una cerniera da cui posso
 ricavare una equazione ausiliaria.



$$\begin{cases}
 a^1 + a^2 = 0 \\
 a^3 + a^4 + 4P = 0 \\
 M_1 = 0 \Rightarrow +a^2 l + P l + P 2l + P 3l + a^4 3l = 0 \\
 M_5 = 0 \Rightarrow P l + a^4 l = 0
 \end{cases}$$

$$\begin{cases}
 a^1 = -a^3 = 3P \\
 a^2 = -4P - a^4 = -4P + P = -3P \\
 a^3 = -6P - 3a^4 = -6P + 3P = -3P \\
 a^4 = -P
 \end{cases}$$

→ ASSEIO STATICO TRAVATURA ✓



Verifiche ✓

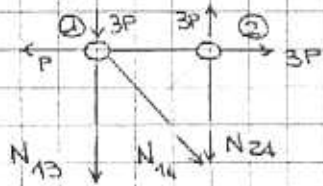
1) An dimensionale:

$$[a^1] = [a^2] = [a^3] = [a^4] = [P] = [F] ✓$$

2) Equilibrio: ✓

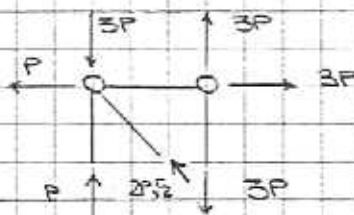
$$\begin{cases} P + P + P + P - 3P - P = 0 ✓ \\ 3P - 3P = 0 ✓ \\ M_G = 0 \quad PE + 2PE + 3PE - \underbrace{3P \cdot 3E}_{-9PE} + 3PE = 0 ✓ \\ M_S = 0 \quad PE + 2PE + 3PE - \underbrace{3P \cdot 2E}_{-6P} = 0 ✓ \end{cases}$$

• Taglio con una sezione di Ritter e aste 13, 24, 14



$$\begin{cases} M_A = 0 \quad \left\{ \begin{aligned} -3PE + 3PE + PE + N_{13}E &= 0 \\ -N_{24}E + 3PE &= 0 \end{aligned} \right. \\ H_{down} \quad \left\{ \begin{aligned} N_{14} \frac{\sqrt{2}}{2} + 3P - P &= 0 \end{aligned} \right. \end{cases}$$

$$\begin{cases} N_{24} = 3P ✓ \\ N_{14} = -2P\sqrt{2} ✓ \\ N_{13} = -P ✓ \end{cases}$$

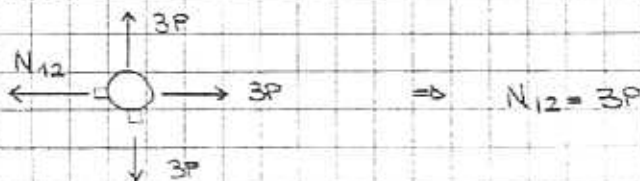


Verifiche:

$$\begin{cases} 3P + P + 2P - 3P - 3P = 0 ✓ \\ 2P + P - 3P = 0 ✓ \end{cases}$$

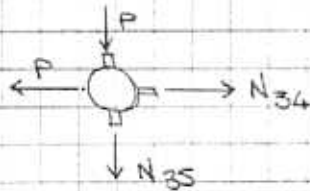
• Analisi dei nodi:

Nodo ②



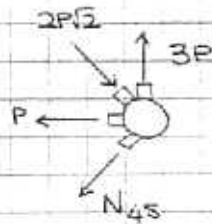
aste	N°	
12	3P	tirante
24	3P	tirante
14	$-2P\sqrt{2}$	puntone
13	-P	puntone
34	P	tirante
35	-P	puntone
45	$P\sqrt{2}$	tirante
56	0	
57	0	
67	P	tirante

Nodo ③



$$\begin{cases} N_{34} = P \\ N_{35} = -P \end{cases}$$

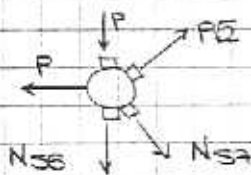
Nodo ④



$$3P - 2P - N_{45} \frac{\sqrt{2}}{2} = 0$$

$$\Rightarrow N_{45} = P \frac{2}{\sqrt{2}} = P\sqrt{2}$$

Nodo ⑤



$$P - P - N_{57} \frac{\sqrt{2}}{2} - N_{56} = 0$$

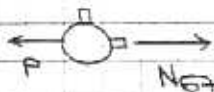
$$N_{57} \frac{\sqrt{2}}{2} + P - P = 0$$

\Leftrightarrow

$$N_{57} = 0$$

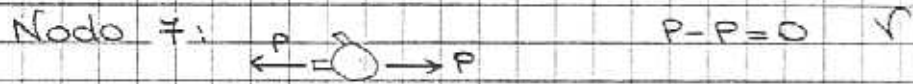
$$N_{56} = 0$$

Nodo ⑥

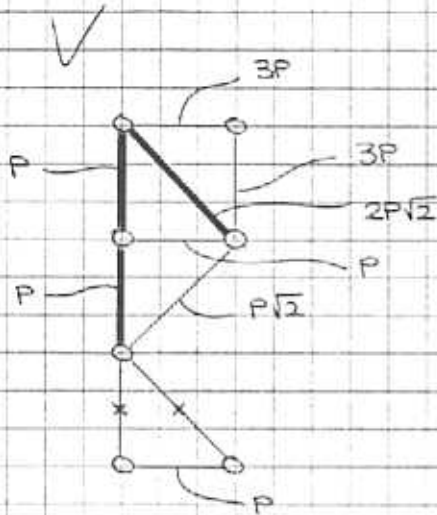


$$N_{67} = P$$

- Verifico i miei risultati con l'equilibrio del nodo 7:



- Disegno il diagramma della caratteristica di sollecitazione Normale: \checkmark



Avendo tutte aste, su di esse Momento e Taglio saranno nulli.