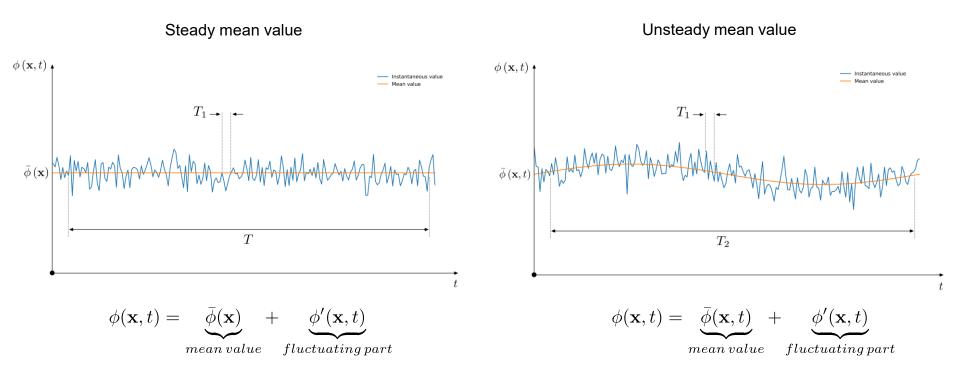
Roadmap to Lecture 5

- 1. Governing equations of fluid dynamics
- 2. RANS equations Reynolds averaging
- 3. The Boussinesq hypothesis
- 4. The gradient diffusion hypothesis
- 5. Sample turbulence models
- 6. Quick review of solution methods for the governing equations of fluid dynamics
- 7. What is Ansys Fluent? Executive summary

Instantaneous fluctuations – Removing small scales



- We have seen that turbulent flows are characterize by instantaneous fluctuations of velocity, pressure, and all transported quantities.
- In most engineering applications is not of interest resolving the instantaneous fluctuations.
- To avoid the need to resolve the instantaneous fluctuations (or small scales), two methods can be used:
 - Reynolds averaging.
 - · Filtering.
- If you want to resolve all scales, you conduct DNS simulations, which are computational expensive.

Instantaneous fluctuations – Removing small scales

- Two methods can be used to eliminate the need to resolve the small scales:
 - Reynolds averaging (RANS/URANS):
 - All turbulence scales are modeled.
 - Can be 2D and 3D.
 - Can be steady or unsteady.
 - Filtering (LES/DES):
 - Resolves large eddies.
 - Models small eddies.
 - Intrinsically 3D and unsteady.
- Both methods introduce additional terms in the governing equations that must be modeled.
 - These terms are related to the instantaneous fluctuations.
- The final goal of turbulence modeling is to find the closure equations to model these additional terms (usually a stress tensor).

Overview of the main turbulence modeling approaches

MODELING APPROACH

RANS

Reynolds-Averaged Navier-Stokes equations

URANS

Unsteady Reynolds-Averaged Navier-Stokes equations

- Many more acronyms that fit between RANS/URANS and SRS.
- Some of the acronyms are used only to differentiate approaches used in commercial solvers.

PANS, SAS, RSM, EARSM, PITM, SBES, ELES

DES

Detached **E**ddy **S**imulations

LES

Large Eddy Simulations

DNS

Direct Numerical Simulations

ncreasing computational cost

SRS Scale-Resolving Simulations

increasing modelling and complexity mathematica

Turbulence modeling – Starting equations

$$\begin{aligned} \mathbf{Exact \, NSE} & \left\{ \begin{array}{l} \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \\ \frac{\partial \left(\rho \mathbf{u} \right)}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \nabla \cdot \tau + \mathbf{S_u} \\ \frac{\partial \left(\rho e_t \right)}{\partial t} + \nabla \cdot (\rho e_t \mathbf{u}) = -\nabla \cdot q - \nabla \cdot (p \mathbf{u}) + \boldsymbol{\tau} \boldsymbol{:} \nabla \mathbf{u} + \mathbf{S}_{e_t} \\ + \end{aligned} \right. \\ & + \end{aligned}$$

Additional equations to close the system (thermodynamic variables)

Additional relationships to relate the transport properties

Additional closure equations for the turbulence models

- Turbulence models equations cannot be derived from fundamental principles.
- All turbulence models contain some sort of empiricism.
- Some calibration to observed physical solutions is contained in the turbulence models.
- Also, some intelligent guessing is used.
- A lot of uncertainty is involved!

Incompressible RANS equations

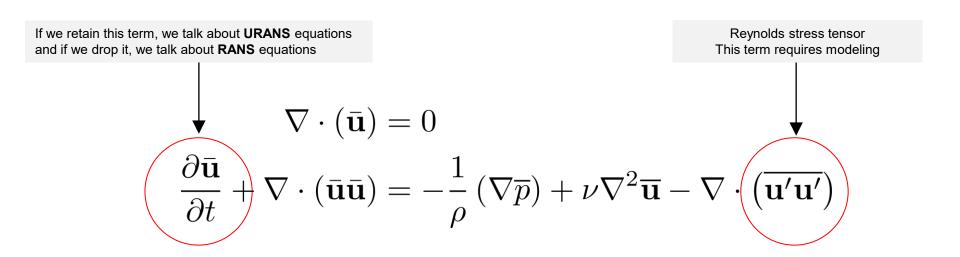
- Let us write down the governing equations for an incompressible flow.
- When conducting DNS simulations (no turbulence models involved), this is our starting point,

$$\nabla \cdot (\mathbf{u}) = 0$$
$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u}\mathbf{u}) = \frac{-\nabla p}{\rho} + \nu \nabla^2 \mathbf{u}$$

- These are the exact governing equations, where we have not introduced approximations.
- Sometimes these equations are referred as the laminar Navier-Stokes equations.
- This does not mean that this set of equations are only valid to laminar regime. They are valid for laminar and turbulent regimes.
- But if you use this set of equations in turbulent regime, you need to resolve all turbulent scales (in space and time), and this requires very fine meshes and very small time-steps.

Incompressible RANS equations

When using RANS/URANS turbulence models, we use the following governing equations,



- In these equations, the overbar represents mean quantities and the prime symbol represent fluctuating quantities.
- In this set of equations, we have not introduced approximations to model the fluctuations.
 - These are the exact RANS/URANS equations.

Incompressible RANS equations

The previous set of equations ca be rewritten as,

$$\begin{split} \nabla \cdot (\bar{\mathbf{u}}) &= 0 \\ \frac{\partial \bar{\mathbf{u}}}{\partial t} + \nabla \cdot (\bar{\mathbf{u}}\bar{\mathbf{u}}) &= -\frac{1}{\rho} \left(\nabla \overline{p} \right) + \nu \nabla^2 \overline{\mathbf{u}} + \frac{1}{\rho} \nabla \cdot \boldsymbol{\tau}^R \end{split}$$

• Where au^R is the Reynolds stress tensor, and it can be written as,

$$\tau^{R} = -\rho \left(\overline{\mathbf{u}' \mathbf{u}'} \right) = - \begin{pmatrix} \rho \overline{u' u'} & \rho \overline{u' v'} & \rho \overline{u' w'} \\ \rho \overline{v' u'} & \rho \overline{v' v'} & \rho \overline{w' v'} \\ \rho \overline{w' u'} & \rho \overline{w' v'} & \rho \overline{w' w'} \end{pmatrix}$$

Incompressible RANS equations

- The Reynolds stress tensor $\boldsymbol{\tau}^R$ represents the transfer of momentum due to turbulent fluctuations.
- It correlates the velocity fluctuations.

$$\tau^{R} = -\rho \left(\overline{\mathbf{u}' \mathbf{u}'} \right) = - \begin{pmatrix} \rho \overline{u' u'} & \rho \overline{u' v'} & \rho \overline{u' w'} \\ \rho \overline{v' u'} & \rho \overline{v' v'} & \rho \overline{w' v'} \\ \rho \overline{w' u'} & \rho \overline{w' v'} & \rho \overline{w' w'} \end{pmatrix}$$

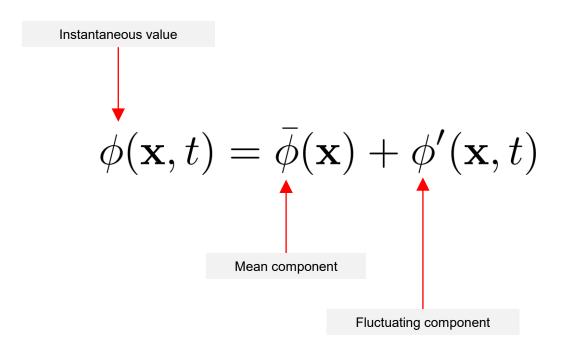
- The Reynolds stress tensor is symmetric; therefore, it has six components.
- The diagonal represents normal stresses and the off-diagonal shear stresses.
- Notice that the Reynolds stress tensor is not actually a stress, it must be multiplied by density in order to have dimensions corresponding to stresses.
- The RANS/URANS approach to turbulence modeling requires the Reynolds stresses to be appropriately modeled.

Incompressible RANS equations

- To derive the incompressible RANS equations, we need to apply Reynolds averaging to the governing equations.
- Reynolds averaging simple consists in:
 - Splitting the instantaneous value of the primitive variables into a mean component and a fluctuating component (Reynolds decomposition).
 - Averaging the quantities (time average, spatial average, or ensemble average).
 - Applying a few averaging rules to simplify the equations.
- When we use Reynolds averaging, we are taking a statistical approach to turbulence modeling.
- When we do DNS, we take a deterministic approach to turbulence modeling.
- Usually, we are interested in the mean behavior of the flow.
- Therefore, by applying Reynolds averaging, we are only solving for the averaged variables and the fluctuations are modeled.

Incompressible RANS equations

 The Reynolds decomposition consists in splitting the instantaneous value of a variable into a mean component and a fluctuating component, as follows,



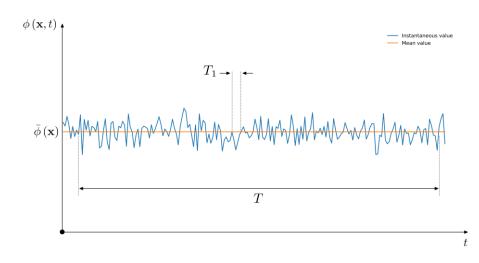
- In our notation, the overbar represents the average (or mean) value, and the prime (or apostrophe) represents the fluctuating part.
- We will use this notation consistently during the lectures.
- But have in mind that you will find different notations in literature.

Incompressible RANS equations

To compute the average (or mean) quantities, we can use time averaging,

$$\bar{\phi}(\mathbf{x}) = \lim_{T \to \infty} \frac{1}{T} \int_{t}^{t+T} \phi(\mathbf{x}, t) dt$$

- Here, T represents the averaging interval. This interval must be large compared to the typical time scales of the fluctuations so it will yield to a stationary state.
- Time averaging is appropriate for stationary turbulence or slowly varying turbulent flows, i.e., a turbulent flow that, on average, does not vary much with time.
- Notice that we are not making the distinction between steady or unsteady flow.
- We are only saying that if we take the average between different ranges or values of t, we will get approximately the same mean value.
- The time average can be in time (unsteady simulations) or iterative (steady simulations).



$$\phi(\mathbf{x},t) = \underbrace{\bar{\phi}(\mathbf{x})}_{mean\ value} + \underbrace{\phi'(\mathbf{x},t)}_{fluctuating\ par}$$

Incompressible RANS equations

- We can also use spatial averaging and ensemble averaging.
- Spatial averaging is appropriate for homogenous turbulence and is defined as follows,

$$\bar{\phi}(t) = \lim_{V \to \infty} \frac{1}{V} \int_{V} \phi(\mathbf{x},t) dV$$
 Volume of the domain

• Ensemble averaging is appropriate for unsteady turbulence.

$$ar{\phi}(\mathbf{x},t) = \lim_{N o \infty} rac{1}{N} \sum_{i=1}^N \phi(\mathbf{x},t)$$

- In ensemble averaging, the number or realizations (or experiments) must be large enough to eliminate the effects of fluctuations.
- This type of averaging can be used with steady or unsteady flows.

Incompressible RANS equations

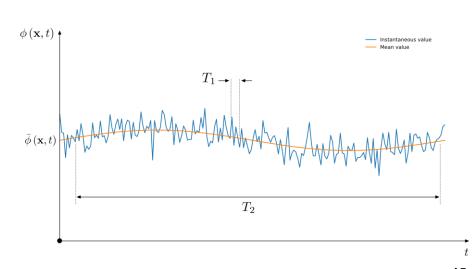
If the mean quantities varies in time, such as,

$$\phi(\mathbf{x},t) = \bar{\phi}(\mathbf{x},t) + \phi'(\mathbf{x},t)$$

We simple modify time averaging, as follows,

$$\bar{\phi}(\mathbf{x},t) = \lim_{T \to \infty} \frac{1}{T} \int_{t}^{t+T} \phi(\mathbf{x},t)dt \qquad T_1 << T << T_2$$

- Where T₂ is the time scale characteristic of the slow variations in the flow that we do not wish to regard as belonging to the turbulence.
- In this kind of situations, it might be better to use ensemble averaging.
- However, ensemble averaging requires running many experiments. This approach is better fit for experiments as CFD is more deterministic.
- Ensemble average can also be used when having periodic signal behavior. However, you will need to run for long times in order to take good averages.
- Another approach is the use of phase averaging.



Incompressible RANS equations

- Any of the previous time averaging rules can be used without loss of generality.
- But from this point on, we will consider only time averaging.
- Before continuing, let us recall a few averaging rules that we will use when deriving the RANS equations.

$$\bar{\phi}' = 0,$$

$$\bar{\bar{\phi}} = \bar{\phi},$$

$$\bar{\bar{\phi}} = \bar{\bar{\phi}},$$

$$\bar{\phi} = \bar{\bar{\phi}} + \bar{\phi}' = \bar{\phi},$$

$$\bar{\phi} + \bar{\varphi} = \bar{\phi} + \bar{\varphi},$$

$$\bar{\bar{\phi}} = \bar{\bar{\phi}} \bar{\varphi} = \bar{\phi} \bar{\varphi},$$

$$\bar{\bar{\phi}} = \bar{\bar{\phi}} \bar{\varphi} = \bar{\phi} \bar{\varphi},$$

$$\bar{\bar{\phi}} = \bar{\phi} \bar{\varphi}' = 0,$$

$$\overline{\phi\varphi} = \overline{(\bar{\phi} + \phi')(\bar{\varphi} + \varphi')}$$

$$= \overline{\phi}\bar{\varphi} + \overline{\phi}\varphi' + \overline{\varphi}\phi' + \phi'\varphi'$$

$$= \overline{\phi}\bar{\varphi} + \overline{\phi}\varphi' + \overline{\varphi}\phi' + \overline{\phi}\varphi'$$

$$= \overline{\phi}\bar{\varphi} + \overline{\phi'\varphi'},$$

$$\overline{\phi'^2} \neq 0,$$

$$\overline{\phi'\varphi'} \neq 0,$$

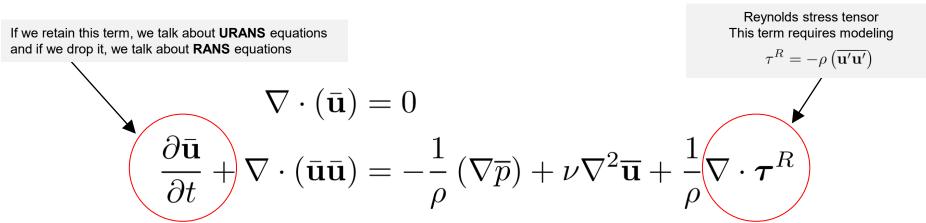
$$\overline{\int \phi ds} = \int \bar{\phi} ds$$

Incompressible RANS equations

 Let us recall the Reynolds decomposition for the primitive variables of the incompressible Navier-Stokes equations (NSE),

$$\mathbf{u}(\mathbf{x}, t) = \bar{\mathbf{u}}(\mathbf{x}) + \mathbf{u}'(\mathbf{x}, t),$$
$$p(\mathbf{x}, t) = \bar{p}(\mathbf{x}) + p'(\mathbf{x}, t)$$

 By substituting the previous equations into the incompressible NSE, using the previous averaging rules, and doing some algebra, we arrive to the incompressible RANS/URANS equations,



Incompressible RANS equations

• The exact RANS equations are very similar to the exact Navier-Stokes equations.

$$\nabla \cdot (\mathbf{u}) = 0$$
$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u}\mathbf{u}) = \frac{-\nabla p}{\rho} + \nu \nabla^2 \mathbf{u}$$

Exact Navier-Stokes equations.

No turbulence models are being used.

These equations are valid for DNS.

$$\nabla \cdot (\bar{\mathbf{u}}) = 0$$

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + \nabla \cdot (\bar{\mathbf{u}}\bar{\mathbf{u}}) = -\frac{1}{\rho} (\nabla \bar{p}) + \nu \nabla^2 \bar{\mathbf{u}} + \frac{1}{\rho} \nabla \cdot \boldsymbol{\tau}^R$$

Exact RANS/URANS equations

- The differences are that all quantities have been averaged in the exact RANS equations (the overbar over the primitive variables).
- And the appearance of the Reynolds stress tensor $\, au^R \,$.

Incompressible RANS equations

Notice that the Reynolds stress tensor $\, au^R\,$ is not actually a stress, it must be multiplied by density in order to have dimensions corresponding to stresses,

Vector notation

$$\boldsymbol{ au}^R = -\rho \left(\overline{\mathbf{u}'\mathbf{u}'} \right)$$

Index notation

$$\tau_{ij}^{R} = -\rho \left(\overline{u_i' u_j'} \right)$$

- Also notice that in the literature, the Reynolds stress tensor $\, au^R\,$ is defined as shown here, as well as with the opposite sign, and sometimes without the density included in the definition.
- This different terminology does not matter, as long as consistency is maintained throughout the derivation.
- From now on, we will use consistently this definition.

Incompressible RANS equations

As previously mentioned, the Reynolds stress tensor $\, au^R\,$ arises from the Reynolds averaging and it can be written as follows,

$$\tau^{R} = -\rho \left(\overline{\mathbf{u}' \mathbf{u}'} \right) = - \begin{pmatrix} \rho \overline{\underline{u}' u'} & \rho \overline{\underline{u}' v'} & \rho \overline{\underline{u}' w'} \\ \rho \overline{\underline{v}' u'} & \rho \overline{\underline{v}' v'} & \rho \overline{\underline{w}' v'} \\ \rho \overline{\underline{w}' u'} & \rho \overline{\underline{w}' v'} & \rho \overline{\underline{w}' w'} \end{pmatrix}$$

$$\mathbf{u} = \begin{bmatrix} \mathbf{u} \\ \mathbf{v} \end{bmatrix} \begin{bmatrix} \mathbf{u} & \mathbf{v} & \mathbf{u} \end{bmatrix} = \begin{bmatrix} \mathbf{u}^{2} & \mathbf{u} \mathbf{v} & \mathbf{u} \mathbf{w} \\ \mathbf{v} \mathbf{u} & \mathbf{v}^{2} & \mathbf{v} \mathbf{w} \\ \mathbf{w} \mathbf{u} & \mathbf{w} \mathbf{v} & \mathbf{w}^{2} \end{bmatrix}$$

- In CFD we do not want to resolve the velocity fluctuations as it requires very fine meshes and small time-steps.
- The RANS/URANS approach to turbulence modeling requires the Reynolds stresses to be appropriately modeled.
- The rest of the terms appearing in the governing equations, can be computed from the mean flow.

- The Reynolds stress tensor τ^R represents the transfer of momentum due to turbulent fluctuations.
- The Reynolds stress tensor is responsible for the increased mixing and larger wall shear stresses.
- Remember, increased mixing and larger wall shear stresses are properties of turbulent flows.
- The RANS/URANS approach to turbulence modeling requires the Reynolds stresses to be appropriately modeled.
- The question now is, how do we model the Reynolds stress tensor au^R ?

- It is possible to derive a set of governing equations for the Reynolds stress tensor au^R .
 - Six new equations as the tensor is symmetric.
- This approach is known as Reynolds stress models (RSM), which we will address in Lecture 6.
- Probably, this is the most physically sound RANS model (RSM) as it avoids the use of hypothesis/assumptions to model the Reynolds stress tensor.
- However, it is much simpler to model the Reynolds stress tensor.
- The most widely hypothesis/assumption used to model the Reynolds stress tensor is the Boussinesq hypothesis, that we will study in next section.

- We just outlined the incompressible RANS equations.
- The compressible RANS equations are similar.
- But to derive them, we use Favre average (which can be seen as a mass-weighted averaging)
 and a few additional averaging rules.
- If we drop the time derivative in the governing equations, we are dealing with steady turbulence.
- On the other hand, if we keep the time derivative, we are dealing with unsteady turbulence.

- If you can afford it, ensemble averaging is recommended.
- But have in mind that CFD is deterministic, so you should start each realization using different initial conditions and boundary conditions fluctuations to obtain different outcomes.
- In CFD time average (steady or unsteady) is preferred.
- The derivation of the LES equations is very similar, but instead of using averaging, we filter the equations in space, and we solve the temporal scales.
- LES/DES models are intrinsically unsteady and three-dimensional.
- We will address LES/DES methods in Lecture 10.

Scalar transport equation

- Evolution and transport of scalar fields, such as temperature, internal energy, species concentration, and so on, can also be modeled in RANS/URANS.
- The exact scalar transport equation of a scalar quantity ϕ (no models used), can be written as follows.

$$\nabla_t \rho \phi + \nabla \cdot \rho \mathbf{u} \phi - \nabla \cdot \Gamma_\phi \nabla \phi = S_\phi$$

- Where Γ_{ϕ} is the molecular (or laminar diffusion) coefficient.
- To derive the exact scalar transport RANS/URANS equation, we proceed in the same way as for the incompressible exact RANS/URANS Navier-Stokes equations.
- Let us define the Reynolds decomposition for the velocity vector **u** and the scalar ϕ , such as,

$$\mathbf{u} = \overline{\mathbf{u}} + \mathbf{u}'$$

$$\mathbf{u} = \overline{\mathbf{u}} + \mathbf{u}'$$
$$\phi = \overline{\phi} + \phi'$$

Scalar transport equation

Introducing the Reynolds decomposition and time averaging the whole equation, we obtain

$$\nabla_{t} \rho \overline{(\overline{\phi} + \phi')} + \nabla \cdot \rho \overline{(\overline{\mathbf{u}} + \mathbf{u}')(\overline{\phi} + \phi')} - \nabla \cdot \Gamma_{\phi} \nabla \overline{(\overline{\phi} + \phi')} = S_{\phi}$$

Let us define the following averaging rules,

$$\bar{\phi}' = 0,$$

$$\bar{\bar{\phi}} = \bar{\phi},$$

$$\bar{\bar{\phi}} = \bar{\bar{\phi}},$$

$$\bar{\phi} = \bar{\bar{\phi}} + \bar{\phi}' = \bar{\phi},$$

$$\bar{\phi} + \bar{\varphi} = \bar{\phi} + \bar{\varphi},$$

$$\bar{\bar{\phi}} = \bar{\bar{\phi}} \bar{\bar{\phi}} = \bar{\phi} \bar{\bar{\phi}},$$

$$\bar{\bar{\phi}} = \bar{\bar{\phi}} \bar{\bar{\phi}} = \bar{\phi} \bar{\bar{\phi}},$$

$$\bar{\bar{\phi}} = \bar{\phi} \bar{\bar{\phi}}' = 0,$$

$$\bar{\bar{\phi}} = \bar{\phi} \bar{\bar{\phi}} = 0,$$

$$\bar{\bar{\phi}} = 0,$$

$$\bar{\bar$$

$$\overline{\phi\varphi} = \overline{(\bar{\phi} + \phi')(\bar{\varphi} + \varphi')}$$

$$= \overline{\phi}\overline{\phi} + \overline{\phi}\varphi' + \overline{\varphi}\phi' + \phi'\varphi'$$

$$= \overline{\phi}\overline{\phi} + \overline{\phi}\varphi' + \overline{\varphi}\phi' + \overline{\phi}\varphi'$$

$$= \overline{\phi}\overline{\phi} + \overline{\phi'\varphi'},$$

$$\overline{\phi'^2} \neq 0,$$

$$\overline{\phi'\varphi'} \neq 0,$$

$$\overline{\int \phi ds} = \int \overline{\phi} ds$$

Scalar transport equation

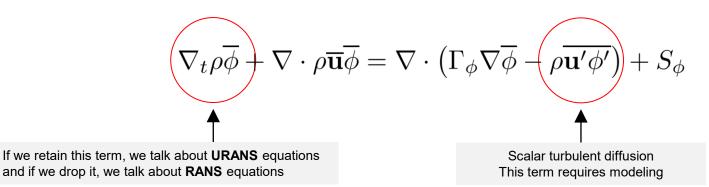
After doing some algebra and using the previously defined averaging rules, we get,

$$\nabla_{t}\rho\left(\overline{\overline{\phi}} + \overline{\cancel{\phi}'}\right) + \nabla \cdot \rho\left(\overline{\overline{\mathbf{u}}\overline{\phi}} + \overline{\overline{\mathbf{u}}}\overline{\phi'} + \overline{\overline{\mathbf{u}'}}\overline{\phi'} + \overline{\overline{\mathbf{u}'}}\overline{\phi'}\right) - \nabla \cdot \Gamma_{\phi}\nabla\left(\overline{\overline{\phi}} + \overline{\cancel{\phi'}}\right) = S_{\phi}$$

After simplifying, we obtain the following equation,

$$\nabla_t \rho \overline{\phi} + \nabla \cdot \rho \left(\overline{\mathbf{u}} \overline{\phi} + \overline{\mathbf{u}' \phi'} \right) - \nabla \cdot \Gamma_{\phi} \nabla \overline{\phi} = S_{\phi}$$

Rearranging and regrouping, we obtain the exact scalar transport RANS/URANS equation,



Scalar transport equation

• The exact RANS/URANS equation is very similar to the exact scalar transport equation.

$$\nabla_t \rho \phi + \nabla \cdot \rho \mathbf{u} \phi - \nabla \cdot \Gamma_\phi \nabla \phi = S_\phi$$

$$\nabla_t \rho \overline{\phi} + \nabla \cdot \rho \overline{\mathbf{u}} \overline{\phi} = \nabla \cdot \left(\Gamma_\phi \nabla \overline{\phi} - \rho \overline{\mathbf{u}' \phi'} \right) + S_\phi$$
Exact scalar transport equation
$$\nabla_t \rho \overline{\phi} + \nabla \cdot \rho \overline{\mathbf{u}} \overline{\phi} = \nabla \cdot \left(\Gamma_\phi \nabla \overline{\phi} - \rho \overline{\mathbf{u}' \phi'} \right) + S_\phi$$

- The differences are that all quantities have been averaged in the exact RANS/URANS equation (the overbar over the primitive variables).
- And the appearance of the extra scalar turbulent diffusion term $\rho \overline{{f u}' \phi'}$.
- As for the incompressible RANS/URANS NSE, this extra term requires modeling.
- The most widely hypothesis/assumption used to model the scalar turbulent diffusion term is the gradient diffusion hypothesis, that we will study in next section.
- As we will see, this hypothesis is very similar to the Boussinesq assumption.